ASME PTC-13 in Action: Practical Approach to Blower System Performance Testing

Hiran de Mel, P.E. and Julie Gass, P.E. *Keynote Speakers*

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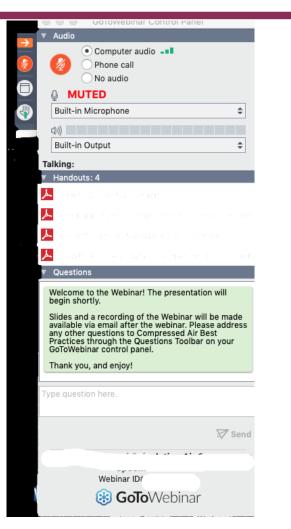
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ASME PTC-13 in Action: Practical Approach to Blower System Performance Testing

Introduction

Blower & Vacuum Best Practices Magazine



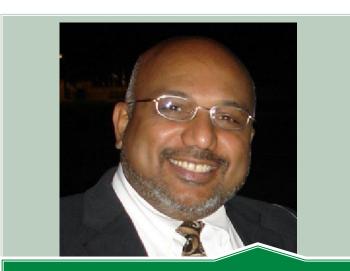
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The Speakers



Hiran de Mel, P.E. Jacobs Keynote Speaker



Julie Gass, P.E. Black & Veatch Keynote Speaker Sponsored by

INOVAIC[®] Geared Centrifugal Blowers





Hiran de Mel

- Brief Introduction to ASME PTC 13
- Specifying PTC 13
- Establishing Performance Points
- Developing a Test Plan
- Witness Test Roles and Responsibilities
- Inovair Blower Test 1
- Things Inovair did well and what can be improved

Julie Gass

- Inovair Blower Test 2
- Test Protocol submittal
- Witness Testing –How to Conduct & What to Look for
- Test Report and Presentation of Results
- Evaluating and Acceptance of Results
- Things Inovair did Well
- Areas for Improvement
- Summary





Overview of ASME PTC 13

"Wire-to-Air Performance Test Code for Blower Systems"

- Developed by: The American Society of Mechanical Engineers (ASME)
- Initiated by: Consortium for Energy Efficiency (CEE) in 2010
- Historical Context:
 - ASME PTC 9 (Displacement Compressors, Vacuum Pumps, Blowers) -First issued in 1915
 - ASME PTC 10 (Compressors and Exhausters) First issued in 1934
- Purpose: Addresses advancements in blower and compressor technology

ASME PTC 13-2018	
Wire-to-Air Performance Test Code for Blower Systems	
Performance Test Codes	
AN AMERICAN NATIONAL STANDARD	SA





Technological and Industry Relevance

- Technological Developments:
 - New mechanisms, control techniques, and integrated systems
- Industry Impact:
 - Focused on wastewater treatment industry
 - Electrical energy usage
- Key Features:
 - Technology-neutral evaluation
 - Wire-to-air power consumption
 - Rigorous, industry-accepted test procedures





Limitations of ASME PTC 13

- Blower Packages with Intercoolers:
 - Not covered; refer to ASME PTC 10
- Blowers with Side Streams:
 - Excluded due to measurement deviations
- Blowers, Fans, and Compressors Applicable when:
 - Gas is air
 - Inlet pressure near atmospheric
 - Pressure ratio ≤ 3.0
 - Covers a range of blower types and applications
- Intent:
 - Standardize performance testing for centrifugal and PD blowers
- Testing <u>without</u> adjustment for uncertainty or including a tolerance, yield the best available indication of the actual performance of the tested equipment





ASME PTC 13 Testing Philosophy - Overview

- Objective:
 - Measure "wire-to-air" performance, focusing on electric power consumption under specified conditions.
- Measurement Procedures:
 - Air Capacity: Inlet volumetric flow rate measured at the blower discharge.
 - Inlet Flow Calculation: Based on delivered mass flow and inlet density.
- Performance Verification:
 - Confirm compliance with specified conditions including flow rate, pressure, and environmental factors.





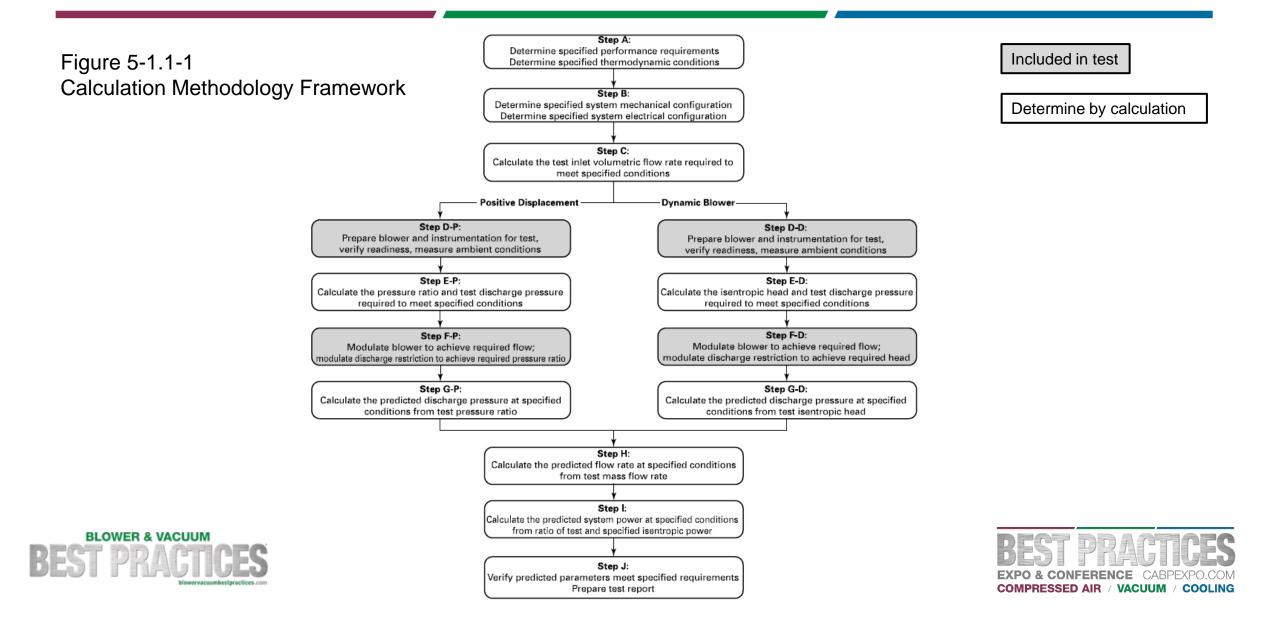
ASME PTC 13 Testing Philosophy - Methodology

- Adjustment of Test Conditions:
 - Match test conditions to specified parameters, emphasizing flow rate and isentropic head/pressure ratio.
- Testing Methodology:
 - Dynamic (Centrifugal) Blowers: Match operating speed with inlet flow rate and isentropic head, using additional flow control methods as needed.
 - Positive Displacement (PD) Blowers: Match operating speed with inlet flow rate and pressure ratio.
- Guidance on Deviations:
 - Detailed directives for acceptable variations in operating conditions and air properties.





Calculation Methodology Framework



Specified Performance Test Points and Conditions

	Continuous	Table 2 Duty Operation	ating Conditio	ns			
	Continuou	100 Hp Blo		/11.5			
Operating Condition ^{(1) (2)}	Inlet Temperature (deg. F)	Inlet Relative Humidity (%)	Discharge Airflow Rate (scfm)	Discharge Pressure (psig)	Total Wire Power (kW)		
Condition 1	95	80%	1,850	6.5	63.5		
Condition 2	95	80%	665	6.5	34.1		
Condition 3	85	80%	1,900	6.5	64.0		
Condition 4	25	0%	685	6.5	36.2		
Condition 5	65	80%	1,960	6.5	N/A		
Condition 6	15	0%	725	6.5	N/A		
Condition 7	95	80%	1,350	4.75	N/A		
Condition 8	95	80%	325	4.75	N/A		
Condition 9	15	80%	1,430	1.25	N/A		
Condition 10	15	0%	355	1.25	N/A		
	-	60 Hp Blov	vers				
Operating Condition (1) (2)	Inlet Temperature (deg. F)	Inlet Relative Humidity (%)	Discharge Airflow Rate (scfm)	Discharge Pressure (psig)	Total Wire Power (kW)		
Condition 1	95	80%	1,350	4.75	42.1		
Condition 2	95	80%	325	4.75	17.2		
Condition 3	85	80%	1,390	4.75	43.2		
Condition 4	25	0%	335	4.75	19.0		
Condition 5	65	80%	1,430	4.75	N/A		
Condition 6	15	0%	355	4.75	N/A		
Condition 7	15	80%	1,430	1.25	N/A		
Condition 8	15	0%	355	1.25	N/A		

Notes:

(1) Each operating condition shall be considered with the discharge pressure and flow measured downstream of the check valve and shall include inlet losses as noted in Table 1.

(2) The blowers shall be capable of continuously operating between Operating Conditions listed. The Total Wire Power performance shall be guaranteed at Conditions 1, 2, 3, and 4 for each blower with no positive tolerance.

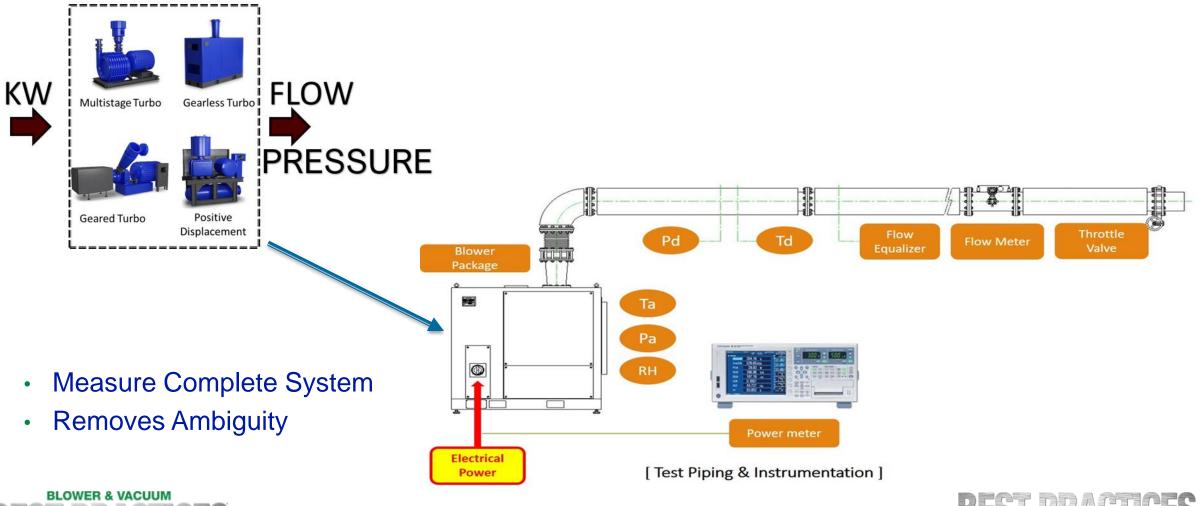


During Testing

- Establish performance envelope as specified
- Measure blower performance at each point at test conditions
- Calculate predicted blower performance at specified site conditions
- Evaluate results



Typical PTC 13 Blower Test Stand Setup

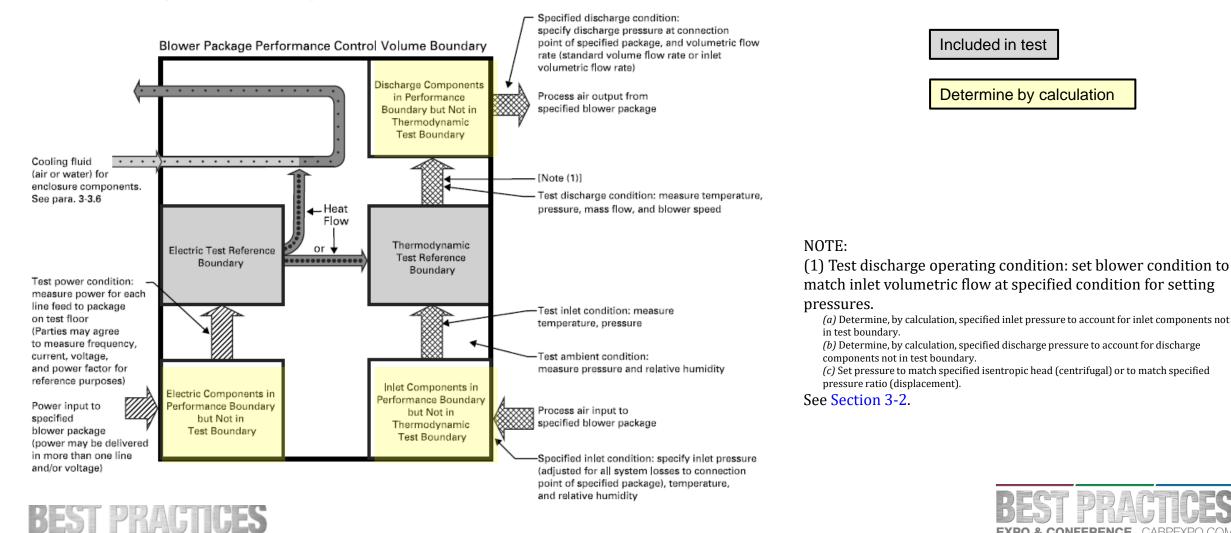


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Control Volume for Thermodynamic and Electrical Reference Boundary

Figure 3-5.2-1 Blower Package Performance Boundary and Internal Reference Boundaries





Specify Thermodynamic Reference Boundary

		Include	d in Performance E	oundary
		Included in	Determine by	Not
		Test	Calculation	Applicable
ı	Inlet filter	Х		
)	Inlet silencer	Х		
;	Discharge silencer			Х
1	Inlet isolation valve			Х
;	Throttling valve			Х
•	After cooler			Х
5	Misc. pipe and fittings	Х		
ı	Inlet air cooler			Х
	Discharge check valve			Х
	Discharge isolation valve			Х
	Enclosure doors or panel openings	Х		
	Estimated system inlet press drop		Х	
5	Additional components not listed included as forming the blower Package			Х

Table 3-5.2-1 – Process and Fluid Components





Specify Electrical Power Reference Boundary

Table 3-5.2-2 – Electrical Power Related Components

		Included	l in Performance E	Boundary
		Included in	Determine by	Not
		Test	Calculation	Applicable
a	Drive motor	X		
b	Motor cooling fan(s)	X		
c	Magnetic Bearing and Controller			X
d	Bearing cooling fan(s)			X
e	Coolant Pumps			X
f	Lubrication Pumps and Accessories			X
g	Heat Exchanger Fans	X		
h	Package Cooling Fan	X		
i	VFD	X		
j	VFD Line Side Power conditioning Equipment			X
j	VFD Load Side Power conditioning Equipment	X		
1	Eddy Current or Variable Speed Clutch			X
k	Operation Control Panel(s)	X		
1	Power/isolation transformers and power supplies	X		
m	Power conditioner			X
n	Blower and motor cooling	X		
0	VFD cooling	X		
р	Additional components not listed included as forming the blower package			Х





Establishing Performance Points, Calculations and Reporting

- Follow PTC-13 calculation procedures:
 - Section 5 Computation of Results
 - Section 6 Report of Results
 - Section 7 Test Uncertainty
 - Mandatory Appendix I Airflow Conversions
 - Nonmandatory Appendices
 - · A Sample Uncertainty Calculations
 - B Sample Calculation: Dynamic Blowers
 - · C Sample Calculation: PD Blowers
 - · D Sample Calculation: Machine Reynolds Number Correction
 - E Sample Calculation: Orifice Flowmeter





Developing a Test Plan

- Develop test plan with test report template
- Develop Test point calculation Sheets
- Develop sample calculations
- Conduct pretest



					In	nvau	r '								
					""		100								
Table 1: Standard Conditions			Table 2:	Specified C					Table 3: 0	onstants					
Temperature	T _{std} 68.0 F Volumetric Flow Rate					9 40,000	1,850 SCFI	4				Rame	1545 348	8 ft-lbf/lbmol-*R	
Pressure	P	14.70 ppia		Inlet Temperature		T Lop	95.0 °F		Universal Ga	niversal Gas Constant		R _{Inv}		8 Btu/Ibmol-*R	
Relative Humidity	RH	36%	Barometric				14.32 osia		Machinela	ouivalent of He		1 DEV		9 ft-lbf/8tu	1
Relative Humicity	M	30%				Pau						,			
Input			Inlet Press			P (10	14.32 psia		-	Conversion, *F	to "R		459.6	+	
			Discharge I			P 4.0	6.50 psig		Proportional	1		9.		1 lbm-ft/lbf-sec ³	
Measured			Relative Hu	-		RH _w	80%		-	sion Constant		n.cr		0 ft-sec/in-min	
			Estimated	Dirty Filter Loss		40;	0.25 psi		Orifice Disch	rge Coefficient		C ₁	0.6	0 initial value	
			Account fo	r Dirty Filter Los	5	P Lap. and	14.07 psia		Uncertainty	of Discharge Coe	fficient	U _c	0.601	6	
			Total Powe	,		٩	63.5 kW		Molecular W	eight of Dry Air		MW _{de}	28.97	0 lbm/lbmol	
									Molecular W	eight of Water \	apor	MW _{ep}	18.01	5 lbm/lbmol	
Table 4: Test Setup Parameters			Table 5:	Test Condit	tions				Table 6: E	stimated O	perating Cond	ition Targets	for Test		
		9.35 in	Ambient Te	mperature		T.,	83.0 17					Brune	-15.751	6	
Inlet Pipe Inner Diameter	0,,	0.779 ft	Barometric			Pau	14.12 psia		Saturated Va	por Pressure Be	ta Coefficients	₿ _{na}	-14.873	++	
Inlet Pipe Inner Area	Au	0.45 ft ²	Relative Hu	midity		ян,	44.20 X					P	-15.200	++	
Assumed Efficiency						-						210		1	н.,
Assumed Ratio of Specific Heats	7						INO	vai	r						
	ĸ						Course	Centrifugal Biv	wara						
Orifice Diameter	d meas	Table 7: Specified Condition Cale	ulations				ondition Calculation	15				t Calculations			
Measured Discharge Pipe Inner Diameter	D	Pressure Ratio	1.000.0	1.48		Estimated Pressure	Fatio	* A.M.S	1.480		Static Discharge	Pressure of Test, pay	0* P.c.m		7.05 prig
		Air Mixture Molecular Weight at Specified Candition	* 10.07	0.0464		Air Minure Melecul	ar Weight at Test Condition	***	0.0554		Discharge Air De	1997 C. 1997	100		0850 35m/1
Measured Discharge Pipe Inner Area	Amer		MW _{en}		broforel			MWate	-	bn/bnai	Iniet Total Teng		T _{UND}		544.2 %
Pipe & Orifice Measurement Temperature	Trees	Air Mixture Density at Specified Condition	P 10	0.0673		Estimated Discharge	Pressure ture Ratio for the Test	Paint	20.90	20.4	Iniet Total Press		P.,.		14.32 poia
Orifice Plate Coefficient of Expansion	0 element	Mass Rew of Mixture	200	142.1	-	Cenditiens		* time	1.182	-	Iniet Tatal Air De	ruity	P.0		0696 (5m/5
Discharge Pipe Coefficient of Expansion	a pipe	Iniet Velocity at Specified Condition	V _i	4,431.2	-	Estimated Discharge Conditions	Temperature for the Text	7.000.000	643.4	-	Discharge Tetal	Temperature	7.414.1		45.32 18
RTD Recovery Factor	4	Pressure Ratio (Tatal Pressures)		1.480	-	Malar Specific Heat		C	-	Paulanai 7	Discharge Tetal		2.0		21.18 pria
Motor Nameplate Base Speed	N,	Molar Specific Heat of Air	* a.m.w	-	Bru/Israel 12	Malar Specific Heat		Card Card	-	Bu/brailt	Discharge Tetal				0650 [bm/7
Gearbox Ratio	R.	Molar Specific Heat of Vapor	facing		Ben Bransi 12	Specific Heat of the		Cambir		Bu/bm/R	Orifice Air Densi		10		0001 bm./
Pulley Ratio		Specific Heat of the Air Minture	family .	-	Bullen 18		ts of the Air Mixture	Kali	1.399		Absolute Vaces		10		96-07 125-04
	^,	Ratio of Specific Heats of the Air Mixture	K minut	1.396		Target Discharge Pre		P sample	21.13		Absolute Viscos				78-47 124-14
Total Ratio	R.,			12.482	# (sl/tsm	Estimated Discharge		Penni	0.0630	lam, M ¹	Abselute Voces		P ===		0E-05 lbm/1
Impeller Diameter (Exducer)	Dimpetier	Ibentropic Head at Specified Condition	W	0.282	WW/Ipre/min	Estimated Discharge		Value	1,931	9/min					
		Isentropic Power at Specified Condition	P	40.1	ww.			P Land, impli	21.12	pris					
						Target Discharge Pre		P Lostowpip	7.00						
		Table 10: Flow Rate of Test				Table 11: Isent	ropic Power of Test	<u></u>			Table 12: Pe	rmissible Devia	tions of Test		
		Test Orifice Diameter	d	5.013	l in	Pressure Ratio (Tota	(Pressures)	* A.M. 1	1.500		Predicted Discha	rge Temperature at 3	Specified .		653.5 18
		Test Discharge Pipe Inner Diameter	0	12.396	i in	Isentropic Head at T	est Canditians	w.,	12.566	A GUIDAN	Canditians			1	193.9 1
		Test Ratio of Orifice and Pipe Diameter	Ø	0.404	-			-		VM/Brev/min	Conditions	inge Air Density at Spe	1 643		0845 (bm/1
		Test Discharge Fige Inner Area	Au	0.530	1 m ²	Isentropic Power at	Test Canditions	P	41.6	ww.		Ratio at Specified Co			1.256
		OrFice Discharge Coefficient	Cu .	0.60141								Ratio at Test Condition			1.265
		Expansion Factor	t _{ee}	0.945		Table 13: Predi	icted Values at Spec	ified Conditio	-		Limit of 95 to 30	5% Flow Rate at Specifie	1.071		10.7%
		Mass Flow of Test	e	146.4	-	Predicted Discharge Canditians	Pressure for the Specified	P 4,0	20.87		Conditions		1.0		.113 efm
		Volumetric Flow Rate of Text	e.,	2.104		Predicted Volumetri	c Fiew Rate for Standard	P 100	6.55			Flow Rate at Test Co-			.104 efm
		Iniet Air Velacity	V is	4,413	R/min R/min	Conditions Predicted System Pa	wer for Specified	e	1.842		Limited from 99		e/		282 149/1
		Discharge Air Velseity Onfloe Air Velseity	V _e		R/min R/min	Conditions Predicted as Percent		P	110.0%			at Specified Condition	n W ₁₀		282 vw//
		OrFice Air Velacity Reynalds Number	V	2 156+05	-	Entire Bower System		1	57.3%		Limited from 10	at Test Conditions	W _{es}		0.204 110/1
		Orifice Discharge Coefficient, Calculated	Cer.	0.60141		Blover thereey		1	63.95		Limited from 30		1 w 1		1.365 RPM
		Orfice Discharge Coefficient, 's Difference	* AUT	0.0015				- 0	5.4			lumber at Specified (andrians Marc		0.726
		2% of Uncertainty	+	0.0129	+							kumber at Test Condi			0.736
		% Difference < 2% of Uncertainty	+	Yes	-	1					Refer to Chart fo				0.010
		Recalculate Flow with Calculated Orffice Dia	harge Coefficient u		-	1									
														-	_

Witness Test Roles and Responsibilities

Role and Responsibilities of the Test Witness

- Specify testing requirements
- Review and approve test plan
- "Bear witness" the test was conducted in conformance with purchase contract requirements
- Ascertain that the proposed test plan meets contract requirements and the requirements of ASME PTC 13
- Make observations to document that the test facilities and conduct of the test are in accordance with contract and ASME PTC 13
- Review the final report from the testing entity to evaluate the reported results represent the experience of the test
- Exercise an opinion as to whether the test results indicate that the blower equipment has met contractual requirements



Role and Responsibilities of the Test Entity

- Prepare a detailed test plan that describes facilities and equipment, methods of testing, predictive calculations and calculation aids, proposed allowable tolerances in test results, and final reporting examples.
- Provide all the equipment, personnel, resources, and logistics to conduct the tests described in the test plan.
- Operate all the equipment involved in the test.
- Collect and record all data.
- Provide a comprehensive report of the test and the site performance results predicted through application of ASME PTC 13.



Inovair Blower Test Stand





- Insulated blower discharge and flow measurement station
- Separate test room with multiple computer screens



- Blower with inlet measurement station
- VFD with control panel

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Things Inovair did well and what can be improved

- Inovair prepared a detailed test plan, test report template and sample calculation sheets
- Sample calculation were submitted with the test protocol in advance
- Multiple resubmittals were required with the test protocol. Not as many with the test report
- Blowers were mechanically pretested and ran in a stable manner during test
- Inovair blower components are manufactured onsite. Other components are sourced locally
- Inovair was able to manufacturer blower components and retest in a week
- Pretest must include performance testing and verification of the test points
- Inovair needs update blower performance information based on ASME PTC 13 testing





Inovair Blowers

2 Stacked Units



Single Unit with VFD







Test Protocol/Procedure Submittal

- Review test protocol submittal at least 30 days in advance
- Schedule meeting with vendor to expedite review if needed
- Submittal should include:
 - Calibration certificates of all instruments to be used dated within previous 12 months
 - Points to be tested guarantee points and 5-point curve if required
 - Test arrangement including flow meter straight runs
 - Flow meter information
 - Data collection sheet
 - Rotor balance reports
- · Several resubmittals were required. Will go more smoothly next time.
- Inovair submitted sample PTC13 calculation which expedited the report submittal. (Recommend requiring sample calculation of one test point for thermodynamic condition correction)





Witness Testing – Performance Guarantees

listed below.

					Performance	e Table			
	A B		С	D	E	F	G	Н	I (G x H)
	Temp (°F)	RH (%)	Total Inlet Flow per Blower (ICFM) ¹	Total Inlet Flow per Blower (SCFM)	Blower Discharge Pressure (psig)	Blower Inlet Pressure Losses (psi)	Guaranteed Power per Blower ² (kW)	Weight Factor (%)	Factored Power per Blower (kW)
1	100	95	1,754	1,533	9.4	0.3	64.2	15	9.6
2	68	80	1,582	1,533	9.4 0.3 62.0	62.0 50		31.0	
3	100	95	1,315	1,150	9.4	0.3	47.5	10	4.8
4	68	80	1,186	1,150	9.4	0.3	46.5	25	11.6
	nt ref		and the second	P LOCK N			in this much	TOTAL	57.0

Vendor shall guarantee the following power numbers for the operating points

Notes:

- 1. Flow shall be measured on the discharge side during testing and corrected to ICFM.
- Guaranteed power consumption indicated shall be the total wire-to-air power consumption of each blower and shall account for any and all losses including, but not limited to, harmonic filters, motor inefficiencies, AFD inefficiencies, cooling fans or cooling pumps, bearing power requirements, and blower controls.
- 3. Performance testing shall test for each specific blower operating point to demonstrate conformance.

2-3. <u>ACCEPTABLE MANUFACTURERS</u>. Blower shall be manufactured by Inovair, without exception:





Witness Testing

Blower on Test Stand



VFD on Test Stand







Witness Testing – How to Conduct

- Witness any required onsite instrument calibration or calibration verification
- Verify calibration certificates are available for all instruments & that they
 match protocol submittal
- Check test stand arrangement to verify it matches protocol submittal
- Review points to be taken and number of readings at each point
- Record test instrument information and verify adequacy including instrument mfr, model, serial, range, division
- Record blower and VFD serial numbers
- Verify location of power measurement & which items are included
- Check route for local direct instrument readings if required





Witness Testing – How to Conduct, cont'd

- Verify thermal stability before starting each reading: No more than 1 deg F change in differential temperature within 5 min
- Start test and timer for readings
- Witness local direct readings and data acquisition readings
- Compare local with DAQ readings
- For centrifugal machines, verify rise to surge requirements are being met
- Take screen shots of DAQ screen
- Request copies of DAQ readings
- If the vendor requires a signature, it should be to verify the readings recorded were the readings witnessed
- Do not sign indicating the unit has passed until there is time to review test report independently in office





Witnessing & Discussion of Readings in Test Lab





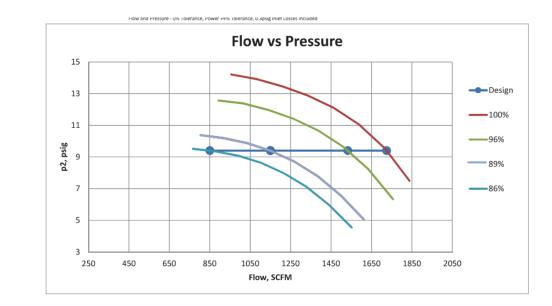


Witness Testing

What to Look for

- While moving up curve, pressure should increase and flow decrease
- Lack of stability between readings at same point
- Objectionable vibration
- Objectionable temperature
- Objectionable noise
- Overhead door opening
- Cooling fan starting or stopping

Example Blower Curve







Test Report & Presentation of Results

- Check sample calculation vs specified site ambient conditions, recorded test lab conditions and PTC13 for methodology
- Compare DAQ readings submitted with screen shots or copies provided at time of test
- Spot check of witnessed local direct instrument values vs values in test report
- Compare local direct readings with DAQ readings (this process should be started during the test)
- Verify required curves have been submitted and that serial numbers are indicated
- Recheck rise to surge requirements are met





- Check flow, pressure, and power vs requirements
- Verify whether power guarantees are met by including weighting factors, present worth factor, etc.





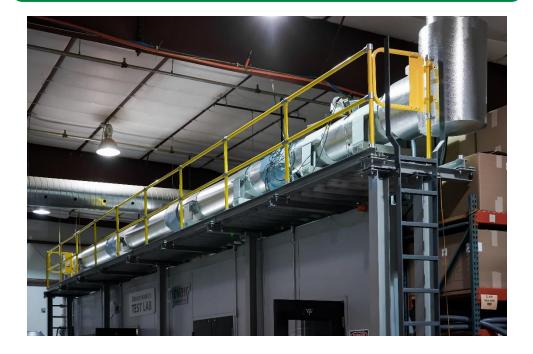
- Blowers ran in a stable manner
- A camera was added to view the instruments on the catwalk from the floor (saved time and enhanced safety)
- Inovair has the capability to modify impellers onsite in case a machine does not perform as required
- Sample calculation was submitted with test protocol in advance of test report
- Initially there were not enough blanks on the data sheet to allow recording of 3 readings at each point but this was quickly corrected





Catwalk Flow Instruments & View in Test Lab

Catwalk with orifice plate instruments



Camera image of catwalk instruments & DAQ screen







Data Collection Sheet

		Test Point D	ata Collection	& Notes					
Blower Package	ver Package Test Point			Date		Time			
Parameter	Symbol	Reading #1	Reading #2	Reading #3	Average Reading	Notes			
			Ambient						
Barometric Pressure	p _a								
Ambient Temperature	τ _σ								
Relative Humidity	RH								
			Inlet						
inlet Pressure	p;								
Inlet Temperature	τ_i								
	-		Discharge						
Discharge Pressure	p _d								
Discharge Temperature	τ_{σ}								
	•	(Drifice & Flow						
Orifice Upstream Pressure	p,								
Orifice Downstream Temperature	Τo								
Orifice Differential Pressure	Δp _o								
Volumetric Flow Rate	<i>q</i> ,								
			Power						
Motor Speed	Ν								
System Power	P 395								
Auxiliary Power	P aux								
Total Power	P tot								





- Multiple resubmittals were required for both the test protocol and test report
- Some of the engineering units did not appear in the test report
- Local, direct reading instruments had to be calibrated onsite on the first day of testing. Temperature instruments were time-consuming requiring 8 hrs for everything
- No local relative humidity gauge or pressure upstream of orifice
- Opening/closing of overhead door or running other blowers in test area can affect thermal equilibrium. Inovair was aware of it.
- Most of these issues will be corrected prior to the next test





Test Instrument Cart







- Before arriving at the manufacturer's shop: Preplanning, reviewing test protocol, pretesting, agreeing on test arrangement, reviewing calibration certificates as well as advance sample calculations (not required but recommended).
- First day at the shop: Performing any needed calibrations, verifying installed instruments and test arrangement.
- All of the above saves time in the long run and results in a better test
- Learning curve for manufacturer and witness: Expect additional time required when a vendor first implements PTC 13 including test protocol submittal, onsite testing, and test report submittal.
- Inovair quickly adjusted to the requirements of PTC13 and a smoother test is anticipated in the future





The Speakers



David Sperber P.E., VP Sales and Marketing



Glen Roderique Sales Engineer for Geared Centrifugal Blowers Sponsored by

INOVAIC[®] Geared Centrifugal Blowers







PTC13 Testing as a Quality Control Tool



PROUDLY MADE IN THE USA

Blowers Built on a History of Performance

Accessible Technologies Inc. (ATI): the market leader in single stage centrifugal compression for 30 Years

1994	1998	2010	2011	2012
ProCharger Superchargers	Airport De-icing	Continuous Duty Industrial	Military Ground Support	Wastewater
30 Years of High Performance - Up to 75 psi and 6,000 scfm	Operating in Extreme Environments	Performance in 24x7 Dirty, Dusty, Environment	99.9% Up-Time for Critical Operations	Highest Efficiency with Leading Reliability

Over 55,000 Geared Centrifugal Units Sold







Vertically Integrated Manufacturer

Inovair is "Buy America" Compliant

- Vertically integrated manufacturer with secure U.S. supply chain
- Factory support from Kansas four building campus headquarters and California regional office with 100 Employees
- Buy America, Build America (BABA) Manufactured in the U.S. with greater than 55 percent of the total cost of all components from the United States

Inovair is the only high efficiency blower designed, manufactured, and supported in the U.S.A.



Inovair PTC 13 Test Cell Implementation

Challenges of Implementation

- Constructing a near lab-level test cell within our existing facility
- Balancing the size of the system for current and future needs
- Sourcing equipment and instrumentation to meet the standard

Rewards/Payback of Implementation

- Improving and supplementing our in-house testing capabilities
- Increasing our awareness, focus on entire blower package/system performance
- Providing the capability for us to meet customer project specifications with less uncertainty





Blower Testing to Validate Efficiency

ASME PTC-13

- Method to validate "wire to air" performance for all power components to substantiate total electrical operating power of the blower package
- Testing used to confirm component selection to optimize efficiency
 - Gearbox Selection based on Speed
 - Impeller Selection from 50+ options
 - VFD manufacturer variations
- Blower Component Quality Control
- Inovair staff member has joined the PTC13 committee.





Design Philosophy Focused on Simplicity

- Integrally geared
 - Robust, reliable and cost effective
 - 16.65:1 step-up ratio
- Speed based control
 - VFD:1800/3600 RPM TEFC 60 Hz Motor
- Designed using off the shelf components
 - 60 Hertz VFD
 - Standard NEMA Frame 1750 RPM Motors
 - PLC (Allen Bradley Compact-Logix)
- Efficiency
 - 50+ impeller stages matched for each application
- Additional Features
 - Quite Operation
 - Internal bypass to allow for additional turn down beyond 50%, turndown to 30%

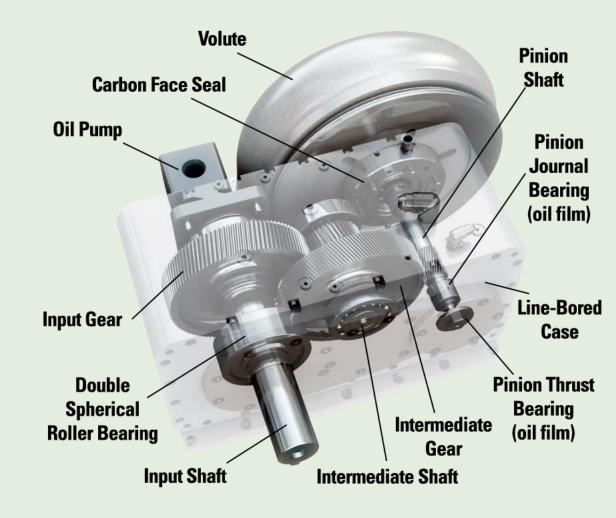
Designed to deliver capital, energy, and maintenance savings

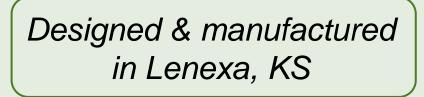
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Integrally-Geared Centrifugal Compressor

- 2-stage gearbox integrated into compressor unit to obtain the designed impeller speed
- Typical operating speeds: 35,000-45,000 rpm
- Designed for up to 22 psi and 60,000 rpm
- Gearboxes rated for up to 600 HP
- High precision gears manufactured to AGMA II standards
- Assemblies balanced to G2.5/G6.3



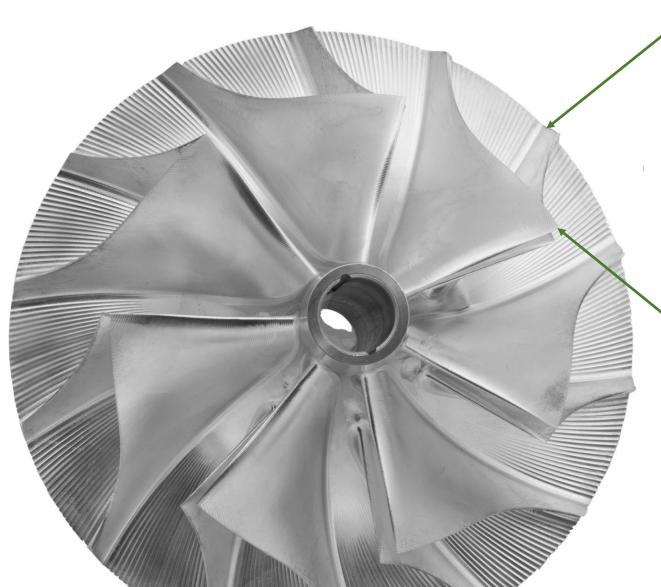




High Efficiency Impellers

Proper relationships between exducer diameter and blade height and inducer diameter must be maintained, along with blade geometry, to ensure highest efficiency.

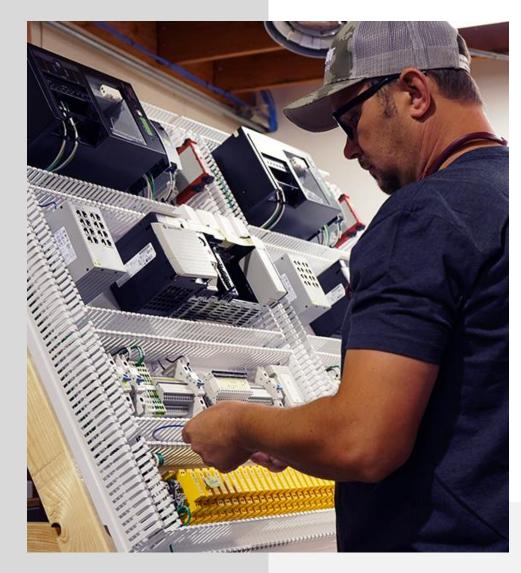
Inovair's impellers are machined at the Kansas City campus using one of three 5-axis CNC mills.



Exducer (outside) diameter and rotational speed (RPM) determine tip speed and thus pressure capability. Pressure increases by a square of the speed.

Inducer diameter and rotational speed effects flow. Flow increases 1:1 with speed.





Versatile Control Systems - constant or varying head applications

- In house UL 508A panel shop
- Standard and custom master control panels
- AB CompactLogix PLC's (custom options available)
- Multiple sensor inputs
- Easily integrates into SCADA or OEM controls
- Accessibility to system
 programming logic

Control Panels are engineered and built in-house



Process Considerations

Airflow Turndown

Inovali

- Aeration Basins
 - Airflow Based on Demand

Project: Morris, IL

515

70.2

32.1

63.7

299

63.3

29.4

Flow vs Pressure

(KW) 56.8

26.3

51.5

245

51.2

24.1

Max. Flow @ Max. Ten

Min. Flow @ Max. Tem

Max. Flow @ Avg. Ten

Max. Flow @ Min. Ten

Min Flow @ Min Ter

Min Flow @ Ave

72%

78%

77%

72%

---- Design

Aero Stage: IF2-23-090

Altitude (ft):

90%

90%

20%

(F)

100

100

50

50

20

20

D.O. Control

inovair

1250

1330

77% 700 9.00

84% 620

91% 1400

79% 665

16

14

12

10

psig

p2,

9.00

9.00

9.00

9.00

9.00

P barer an +7-5% talerance CFM bared an 68F, 36% RH, 14.7 pr

200

400

600

800

Flow, SCFM

1000

1200

1400

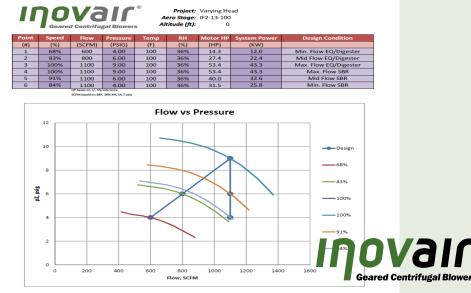
1600

• Lagoons, MBR's, IFAS Systems

- Varying Water Depths
 - Equalization Tanks
 - Sludge Holding Tanks
 - Aerobic Digesters
 - SBR's

VS





Inovair Product Line

Design Ranges

- Airflow up to 12,000 SCFM
- Power from 15 hp to 600 hp
- Pressure up to 22 PSI

Inovair's geared centrifugal blower are designed to deliver capital, energy, and maintenance savings

IO/IM SERIES MACHINE LINEUP







Geared Centrifugal Blowers

THANK YOU!

VISIT US AT INOVAIR.COM

ACCESSIBLE TECHNOLOGIES INC.



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ASME PTC-13 in Action: Practical Approach to Blower System Performance Testing

Q&A

Please submit any questions through the Question Window on your GoToWebinar interface, directing them to Blower & Vacuum Best Practices Magazine. Our panelists will do their best to address your questions and will follow up with you on anything that goes unanswered during this session. **Thank you for attending!**

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PDH Certificates will be e-mailed to Attendees by within 2 days





February 2024 Webinar Centrifugal vs Rotary Screw Air Compressor Performance: Full Load and Part Load Efficiency



Mike Lenti Compressed Air Consultants Keynote Speaker

Thursday, February 8, 2024–2:00 PM EST

Register for free at <u>www.airbestpractices.com/webinars</u>

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